
SHORT
COMMUNICATIONS

Modal Control of a Linear Differential Equation with Incomplete Feedback

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Consider the linear stationary controlled system

$$\dot{x} = Ax + Bu, \quad x \in \mathbf{R}^n, \quad u \in \mathbf{R}^m. \quad (1)$$

Suppose that all coordinates of the state vector x can be measured. Taking a feedback control $u = Ux$, we obtain the closed system

$$\dot{x} = (A + BU)x. \quad (2)$$

The problem of placing the eigenvalues $\lambda_i(A + BU)$, $i = 1, \dots, n$, of system (2) at arbitrary given points is called the *modal control problem*. The term “modal control” is due to the fact that the eigenvalues correspond to components of free motion of the system, sometimes referred to as *modes* [1, p. 5]. A similar problem for a nonstationary system (2) is referred to as the control problem for Lyapunov characteristic exponents. One says that the Lyapunov exponents of system (2) are *globally controllable* if, by using some admissible control, one can bring them to arbitrary given points in \mathbf{R} ; the exponents are said to be *locally controllable* if, by using small-norm controls, one can bring them to arbitrary given points in a neighborhood of the exponents of the nonperturbed system (2) with $U = 0$. We consider only stationary systems. The requirement of complete controllability of system (1) is known to be a necessary and sufficient condition for the global controllability of Lyapunov exponents. For example, consider the single-input n th-order linear differential equation

$$x^{(n)} + a_1 x^{(n-1)} + \dots + a_n x = u, \quad x \in \mathbf{R}, \quad u \in \mathbf{R}. \quad (3)$$

The controlled system (3) is equivalent to the matrix system (1), where A is a Frobenius matrix and $B = e_n$ is the n th column of the identity matrix I . This matrix system is completely controllable, and the control $U = (a_n - \gamma_n, \dots, a_1 - \gamma_1)$ brings the characteristic polynomial of system (3) to an arbitrary given form $p(\lambda) = \sum_{i=0}^n \gamma_i \lambda^{n-i}$ ($\gamma_0 = 1$). Accordingly, the control

$$u = (a_1 - \gamma_1)x^{(n-1)} + \dots + (a_n - \gamma_n)x \quad (4)$$

brings Eq. (3) to an equation with given coefficients γ_i and provides the desired asymptotics of solutions of system (3), (4).

Consider an n th-order object whose input is a linear combination of m signals and their derivatives of order $\leq n - p$. We assume that k distinct linear combinations of the object state z and its derivatives of order $\leq p - 1$ can be measured:

$$\begin{aligned} z^{(n)} + a_1 z^{(n-1)} + \dots + a_n z \\ = b_{p1} v_1^{(n-p)} + b_{p+1,1} v_1^{(n-p-1)} + \dots + b_{n1} v_1 + \dots + b_{pm} v_m^{(n-p)} + \dots + b_{nm} v_m, \end{aligned} \quad (5)$$

$$z \in \mathbf{R}, \quad 1 \leq p \leq n, \quad (6)$$

$$y_i = c_{1i} z + \dots + c_{pi} z^{(p-1)}, \quad i = 1, \dots, k, \quad (6)$$

where $v = \text{col}(v_1, \dots, v_m) \in \mathbf{R}^m$ is the control vector and $y = \text{col}(y_1, \dots, y_k) \in \mathbf{R}^k$ is the output vector. The modal control problem is the problem of constructing an incomplete feedback control $v = Uy$ that brings system (5), (6) to a closed system

$$z^{(n)} + \gamma_1 z^{(n-1)} + \dots + \gamma_n z = 0 \quad (7)$$

with given coefficients. Such a control was constructed in [1, p. 36] for a completely controllable, completely observable object (5), (6) for the case in which $m + k - 1 \geq n$, i.e., the total number of input and output signals exceeds the dimension of the object. (This case is rather trivial.) In the present paper, we obtain a necessary and sufficient condition for the existence of a modal control of system (5), (6) with incomplete feedback $v = Uy$.

On the basis of system (5), (6), we construct matrices $B \in M(n, m)$ and $C \in M(n, k)$ with entries $b_{ij} \equiv 0$, $i = 1, \dots, p-1$, $j = 1, \dots, m$, and $c_{ij} \equiv 0$, $i = p+1, \dots, n$, $j = 1, \dots, k$, where $M(n, k)$ is the space of $n \times k$ matrices. Let $J_0 = I \in M(n, n)$, and let $J_1 \in M(n, n)$ be the matrix whose entries on the first superdiagonal are equal to unity and whose remaining entries are zero. We set $J_q \doteq J_1^q$. The asterisk stands for transposition of matrices. (The transpose of a column vector is a row vector.)

Theorem 1. *Let the feedback $v = Uy$ bring system (5), (6) to the closed system (7). Then the coefficients γ_i of system (7) satisfy the relations $\gamma_i = a_i - \text{Sp } C^* J_{i-1} B U$, $i = 1, \dots, n$.*

The proof is based on the following lemma.

Lemma 1. *Let $D_i = C^* J_i B$, $i \in \{0, \dots, n-1\}$, and $D_i = \{d_{rj}^i\}$, $r = 1, \dots, k$, $j = 1, \dots, m$. Then $d_{rj}^i = \sum_{l=i+1}^n c_{l-i,r} b_{lj}$.*

Proof. For each $i \in \{0, \dots, n-1\}$, we construct the matrix $J_i = \{\alpha_{st}^i\}_{s,t=1}^n$. Then $\alpha_{s,s+i}^i = 1$ for all $s = 1, \dots, n-i$, and the remaining entries α_{st}^i are zero. Let $F_i = C^* J_i$. Then $F_i = \{f_{rl}^i\}$, $r = 1, \dots, k$, $l = 1, \dots, n$, where $f_{rl}^i = \sum_{s=1}^n c_{sr} \alpha_{sl}^i$. Since $\alpha_{l-i,l}^i = 1$ (if $l > i$) and the remaining entries α_{sl}^i are zero (and all α_{sl}^i are zero if $l \leq i$), it follows that $f_{rl}^i = c_{l-i,r} \text{sgn } \max\{0, l-i\}$. Therefore,

$$d_{rj}^i = \sum_{l=1}^n f_{rl}^i b_{lj} = \sum_{l=i+1}^n c_{l-i,r} b_{lj}.$$

The proof of the lemma is complete.

Proof of Theorem 1. Let us compute the trace of the matrix $C^* J_{i-1} B U$. Let $D_{i-1} = C^* J_{i-1} B = \{d_{rj}^{i-1}\} \in M(k, m)$ and $U = \{u_{jr}\} \in M(m, k)$. Then, by Lemma 1,

$$\text{Sp } C^* J_{i-1} B U = \text{Sp } D_{i-1} U = \sum_{r=1}^k \sum_{j=1}^m d_{rj}^{i-1} u_{jr} = \sum_{r=1}^k \sum_{j=1}^m \sum_{l=i}^n c_{l+1-i,r} b_{lj} u_{jr}. \quad (8)$$

Let us substitute the control $v = Uy$ into system (5). We denote the right-hand side of the resulting relation by Δ . Let us show that the coefficient of $z^{(n-i)}$ on the right-hand side coincides with (8), which implies the assertion of the theorem. Since $v_j = \sum_{r=1}^k u_{jr} y_r$ for all $j = 1, \dots, m$ and $y_r = \sum_{s=1}^p c_{sr} z^{(s-1)}$ for $r = 1, \dots, k$, we have

$$\begin{aligned} \Delta &= \sum_{j=1}^m \sum_{l=p}^n b_{lj} v_j^{(n-l)} = \sum_{j=1}^m \sum_{l=p}^n b_{lj} \left(\sum_{r=1}^k u_{jr} y_r \right)^{(n-l)} \\ &= \sum_{j=1}^m \sum_{l=p}^n \sum_{r=1}^k b_{lj} u_{jr} \left(\sum_{s=1}^p c_{sr} z^{(s-1)} \right)^{(n-l)} = \sum_{j=1}^m \sum_{l=p}^n \sum_{r=1}^k \sum_{s=1}^p b_{lj} c_{sr} u_{jr} z^{(n-l+s-1)}. \end{aligned}$$

Let $i = l - s + 1$. Then i ranges from $l - p + 1$ to l . Therefore,

$$\Delta = \sum_{r=1}^k \sum_{j=1}^m \sum_{l=p}^n \sum_{i=l-p+1}^l b_{lj} c_{l+1-i,r} u_{jr} z^{(n-i)}.$$

Note that if i ranges from 1 to $l - p$, then $c_{l+1-i,r} = 0$. Consequently,

$$\Delta = \sum_{r=1}^k \sum_{j=1}^m \sum_{l=p}^n \sum_{i=1}^l b_{lj} c_{l+1-i,r} u_{jr} z^{(n-i)}.$$

Now we note that if l ranges from 1 to $p - 1$, then $b_{lj} = 0$, whence it follows that

$$\Delta = \sum_{r=1}^k \sum_{j=1}^m \sum_{l=1}^n \sum_{i=1}^l b_{lj} c_{l+1-i,r} u_{jr} z^{(n-i)}.$$

We change the summation order, replacing $\sum_{l=1}^n \sum_{i=1}^l$ by $\sum_{i=1}^n \sum_{l=i}^n$; then we obtain

$$\Delta = \sum_{r=1}^k \sum_{j=1}^m \sum_{i=1}^n \sum_{l=i}^n b_{lj} c_{l+1-i,r} u_{jr} z^{(n-i)} = \sum_{i=1}^n z^{(n-i)} \sum_{r=1}^k \sum_{j=1}^m \sum_{l=i}^n c_{l+1-i,r} b_{lj} u_{jr}.$$

The coefficient of $z^{(n-i)}$ coincides with (8). The proof of the theorem is complete.

Let us now find conditions guaranteeing that system (5), (6) has a modal control. We introduce the mapping $\text{vec} : M(n, m) \rightarrow \mathbf{R}^{nm}$ that unwraps every matrix $H = \{h_{ij}\}$, $i = 1, \dots, n$, $j = 1, \dots, m$, into a column vector by the rule

$$\text{vec } H = \text{col}(h_{11}, h_{12}, \dots, h_{1m}, \dots, h_{n1}, \dots, h_{nm}).$$

Note that $\text{Sp}(A^*B) = (\text{vec } A)^* \cdot (\text{vec } B)$ for any matrices $A, B \in M(n, m)$. We construct the matrices

$$C^* J_0 B, \quad \dots, \quad C^* J_{n-1} B \quad (9)$$

and the matrix $P = [\text{vec } C^* J_0 B, \dots, \text{vec } C^* J_{n-1} B] \in M(mk, n)$. Let $a = \text{col}(a_1, \dots, a_n) \in \mathbf{R}^n$.

Theorem 2. *System (5), (6) has a modal control if and only if the matrices (9) are linearly independent, and in this case, the feedback matrix U bringing system (5), (6) to the form (7) with prescribed coefficients is given by (11), where $w = \text{vec } U^*$.*

Proof. System (5), (6) has a modal control if and only if, for each $\gamma = \text{col}(\gamma_1, \dots, \gamma_n) \in \mathbf{R}^n$, there exists a matrix $U \in M(m, k)$ such that

$$\gamma_i = a_i - \text{Sp } C^* J_{i-1} B U = a_i - \text{Sp } U C^* J_{i-1} B.$$

This is a system of n equations with mk unknowns $\{u_{jr}\}$. It can be rewritten in the vector form

$$a - P^* w = \gamma, \quad (10)$$

where $w = \text{vec } U^*$. If the matrices (9) are linearly independent, then $\text{rank } P = n$. In this case, $P^* P$ is a nondegenerate matrix, system (10) is solvable for any γ , and its solution has the form

$$w = P (P^* P)^{-1} (a - \gamma). \quad (11)$$

But if the matrices (9) are linearly dependent, then $\text{rank } P < n$ and system (10) has no solution for the vector $\gamma = a - \beta$, where $\beta \notin \text{Im } P^*$. The proof of the theorem is complete.

Note that in a system with an incomplete feedback, as well as in a system with a complete feedback, the possibility of bringing the system to a prescribed equation is independent of the coefficients a_i of the equation and only depends on the coefficients b_{lj} and c_{sr} of the linear combinations of input and output signals.

Example. Consider system (5), (6) with $n = 6$, $m = 2$, $k = 3$, $z^{VI} = v_1 + v_2'$, $y_1 = z$, $y_2 = z''$, and $y_3 = z^{IV}$. For this system, we construct the matrices B and C . One can readily see that the matrices (9) are linearly independent. Therefore, this system has the modal control $v = Uy$, where

$$U = \begin{pmatrix} -\gamma_6 & -\gamma_4 & -\gamma_2 \\ -\gamma_5 & -\gamma_3 & -\gamma_1 \end{pmatrix}.$$

This example shows that the condition $m + k - 1 \geq n$ can be weakened for system (5), (6). For the existence of a modal control, it is necessary that the dimensions m and k satisfy the condition $mk \geq n$. This readily follows from Theorem 2.

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